

# V(SWR)

#### Mirror, Mirror, Darkly, Darkly



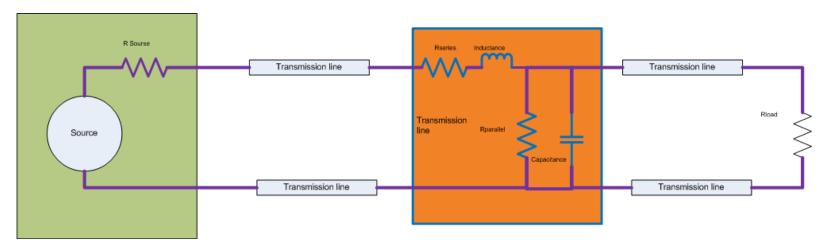
# Question time!!

- What do you think VSWR (SWR) mean to you?
- What does one mean by a transmission line?
  - Coaxial line
  - Waveguide
  - Water pipe
  - Tunnel (Top Gear, The Grand Tour)
- Relative permittivity.
  - Vacuum = 1.00000
  - $Air = \kappa_{air} = 1.0006.$
- Why is the concept of an infinite transmission line of any use?

In SI units, the speed of light in vacuum, c,<sup>[14]</sup> is related to the magnetic constant and the electric constant (vacuum permittivity),  $\varepsilon_0$ , by the definition:

$$c = \frac{1}{\sqrt{\mu_0 \varepsilon_0}}.$$

# **VSWR Schematic**



The elements in the orange box represents the equivelent circuit of a transmission line. This circuit demonstrates that the characteristics of the line are determined by mechanical effects:

Capacitance is proportional to the area divided by the gap.

Inductance is proportional to the number turns and area of the loop

Resistance is determined by the material it is made up of.

**Transmission Line Characteristic** 

Impedance Formula

$$Z_0 = \sqrt{L/C}$$

 $L-unit\ length\ inductance$ 

 $C-unit \ length \ capacitance$ 

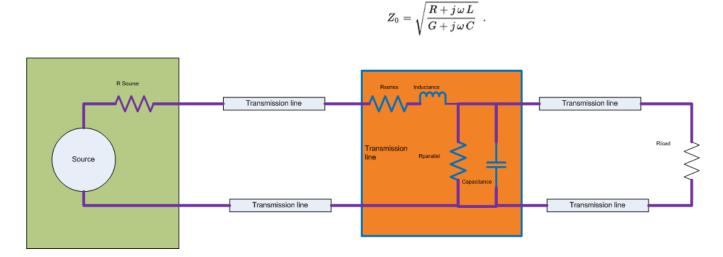
 $Z_0 - characteristic impedence in ohms$ 

# Some Definitions

- What is meant by an infinite transmission line and what does have to matching and hence, VSWR.
  - Any line that is perfectly matched, by definition has VSWR of 1:1
  - A line which has infinite length (free space= $377\Omega$ ).
  - A large attenuator
  - A transmission line can have any impedance.

### **VSWR Waveform**

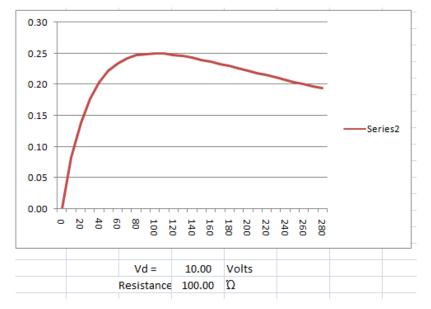
• Circuit

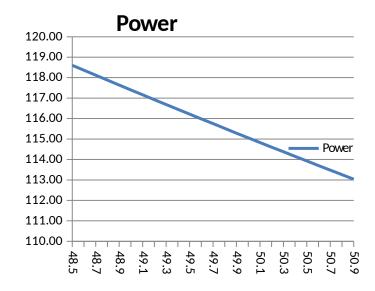


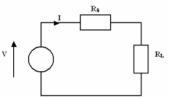
 $Z_{o} \qquad \rho \qquad Z_{L}$ 

# Maximum power transfer theorem

- The theorem shows the maximum power transfer with source and resistance set to  $100\Omega$ 







In the diagram opposite, power is being transferred from the source, with voltage V and fixed source resistance  $R_S$ , to a load with resistance  $R_L$ , resulting in a current I. By Ohm's law, I is simply the source voltage divided by the total circuit resistance:

$$I = rac{V}{R_{
m S}+R_{
m L}}.$$

The power P<sub>L</sub> dissipated in the load is the square of the current multiplied by the resistance:

$$P_{
m L} = I^2 R_{
m L} = igg( rac{V}{R_{
m S} + R_{
m L}} igg)^2 R_{
m L} = rac{V^2}{R_{
m S}^2/R_{
m L} + 2R_{
m S} + R_{
m L}}$$

6

# Some more Definitions

- What is VSWR?
  - VSWR is the acronym for Voltage (Standing Wave Ratio).
  - VSWR has no units, its a ratio of the max and min values of the standing wave.
  - VSVR value can be between 1 to  $\infty$  or 1 to 0.
- Some features of VSWR
  - The max and min occur every  $\frac{1}{4}\lambda$
  - Repeats every  $\frac{1}{2}\lambda$  (Smith chart repeats likewise)
  - Short circuit would give 0 volts and 2\*I amps; zero power
    - Where I and V are the matched currents and voltages
  - Open circuit would give 2\*V and 0 amps; zero power
- SWR meters measure incident and reflected **power**

#### This is based on the Reflection Coefficient (Γ)

• What is the value of VSWR:

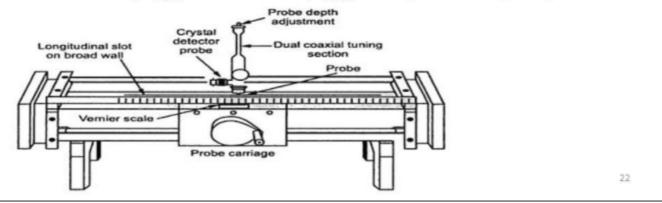
- VSWR = (1- $\Gamma$ )/(1+ $\Gamma$ )

- VSWR:
  - This is based on the derivation of the reflection coefficient (Γ).
  - The reflection coefficient is the ratio of the max reflected voltage to the min reflected voltage.
  - The max and min occur at every quarter wavelength.

# Simple way of measuring VSWR

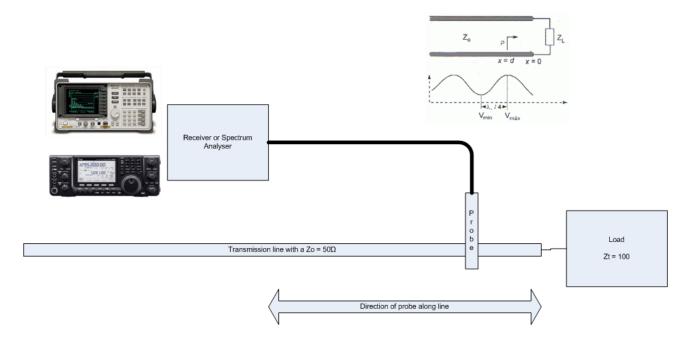
#### **Slotted Line Carriages**

- A slotted line carriage is a microwave instrument which is used to measure:
  - Wavelength
  - · Voltage Standing Wave Ratio (VSWR) and standing wave pattern
  - · Impedance, reflection coefficient and return loss measurement
- It has a coaxial E-field probe which penetrates inside a rectangular waveguides slotted in sections from the outer wall.
- The probe is able to transverse a longitudinal narrow slot and locate the standing waves maxima( $V_{max}$ ) and minima( $V_{min}$ ) along the line giving VSWR.



## VSWR Measurement.

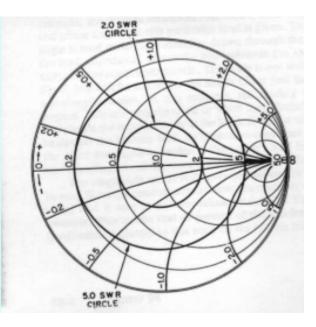
- Receiver approach.
  - It is useful if you know the velocity of propagation of the cable. (A number between 0 and 1)



#### Using a network analyser (Mini MVNA tiny)

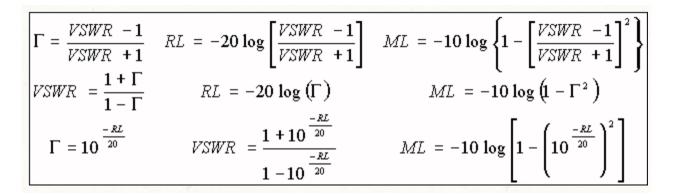
- Frequency range 50MHz to 3GHz
- Cal kit: Short Circuit, Open Circuit and Load.
- Display: Cartesians (XY plot) or Smith chart.
- VSWR requires one port.





## **Useful Formulas**

VSWR to Return loss	
3:1 =	6 dB
2:1 =	9.5 dB
1.5:1 =	14 dB
1.2:1 =	20.8 dB
1.1:1 =	26.4 dB



Definitions:  $\Gamma$  = Reflection coefficient RL = Return loss ML = Mis-Match loss

### **Mis-Match Test Cases**

		Test case 1				1		Test case 2	2				Test case 3			
100	watts		20.00	dBW		100	watts		20.00	dBW		100	watts		20.00	dBW
			50.00	dBm		100			50.00	dBm					50.00	dBm
1																
Returr	n loss		3.00	dB		Return loss			9.50	dB		Retur	n loss		20.80	dB
			50.12	Watts					11.22	Watts					0.83	Watts
Pov	ver					Pov	ver					Pov	wer			
			17.00	dBW					10.50	dBW					-0.80	dBW
					-											
Power transm	nitted to load		49.88	Watts		Power transn	nitted to load		88.78	Watts		Power transn	nitted to load		99.17	Watts
		VSWR =	5.85					VSWR =	2.01					VSWR =	1.20	

## **VSWR** meters

The picture depicts a typical VSWR meter

The important point is that the two scales indicate power. (Incident and reflective)

From these two readings the return loss is calculated.

From the return loss the VSWR is calculated

This calculation is shown in the excel computation below and this is calculated by the meter in the VSWR curves in red and the indicated VSWR is where the two needles cross.



		Fror	n Return	loss to V	SWR				
	incedent	power	100.00	mw		20.00	dBm		
	Reflected	l power	10.00	mw		10.00	dBm		
		mitted wer	90.00	mw		19.54	dBm		
	Return	n loss =	10.00	dB		10.00	dB		t
	Mis-Mat	ch loss =	0.46	dB					
	VSW	/R =	1.92	:1					

# **Common transmission lines**

• If the transmission line is coaxial in construction, the characteristic impedance follows a different equation:

$$d_1$$
  $d_2$ 

$$Z_0 = \frac{138}{\sqrt{k}} \log \frac{d_1}{d_2}$$

Where,

- Z<sub>0</sub> = Characteristic impedance of line
- d1 = Inside diameter of outer conductor
- d<sub>2</sub> = Outside diameter of inner conductor
- k = Relative permittivity of insulation between conductors

Ca	lculation o	f the line	impeadan	ce
	d1 =	3.00	mm	
	d2=	2.00	mm	
	k =	1.00	permitivity	,
	Zo =	24.30		

# **Common transmission lines**

 For a parallel-wire line with air insulation, the characteristic impedance may be calculated as such:
 Calculation of the line impedance



$$Z_0 = \frac{276}{\sqrt{k}} \log \frac{d}{r}$$

Where,

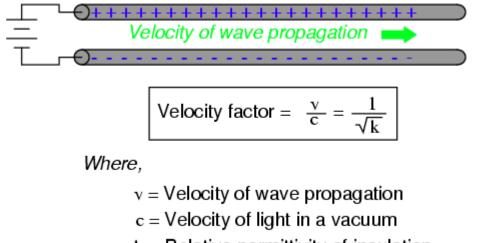
- $Z_0$  = Characteristic impedance of line
  - d = Distance between conductor centers
  - r = Conductor radius
  - k = Relative permittivity of insulation between conductors

Calc	ulation o	f the lin	e impeda	ince
	d =	3.00	mm	
	r =	2.00	mm	
	k =	1.00	permitivi	ty
	Z0 =	48.60		

Calc	ulation of	the line	e impeada	ance
	d =	23.40	mm	
	r =	1.00	mm	
	k =	1.00	permitivi	ty
	Z0 =	377.90		

# Velocity factor

• Velocity factor is purely a factor of the insulating material's relative permittivity (otherwise known as its *dielectric constant*), defined as the ratio of a material's electric field permittivity to that of a pure vacuum. The velocity factor of any cable type—coaxial or otherwise—may be calculated quite simply by the following formula:



k = Relative permittivity of insulation between conductors

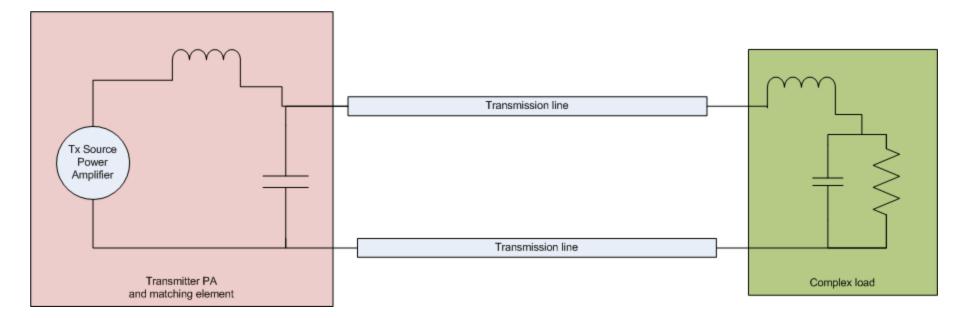
Velocity	y of prop	ogation	
 k =	1.00	permitivity	,

### VSWR and its relationship to Transmitter amplifier

- The transmitter has to get all the power to the antenna structure. (Transmission line and antenna).
- The power amplifier must be matched to the transmission system.
- It must be able withstand full reflected power.
- It must be efficient in the use of input power.

# Transmitter Equivalent Circuit

• The circuit below depicts a typical circuit for a transmitter PA delivering power to a complex load via a transmission line



#### Lattice (bounce) diagram

This is a space/time diagram which is used to keep track of multiple reflections.

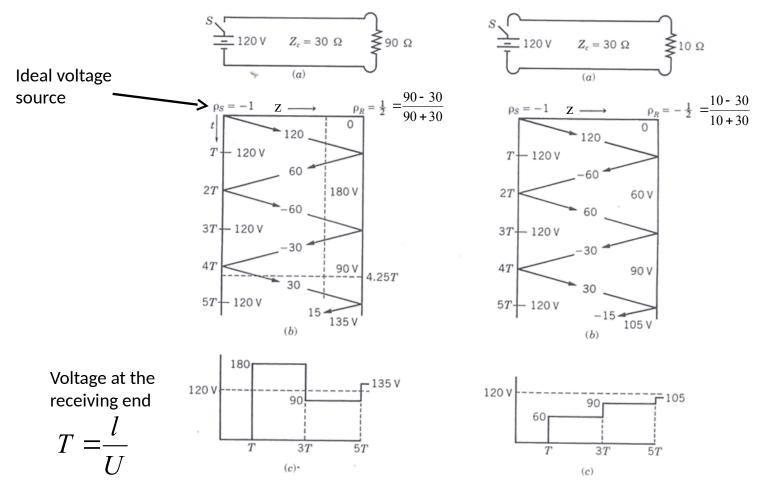


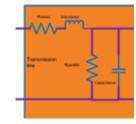
Figure 5.14 Circuit diagram, lattice diagram, and plot of voltage versus time for Example 5.6 where the receiving-end resistance is 90  $\Omega$ .

Figure 5.15 Circuit diagram, lattice diagram, and plot of voltage versus time when the receiving-end resistance for Example 5.6 is changed to 10  $\Omega$ .

# Ladder diagram showing the reflection in a cable driven by an impulse function

			I	VSWR L	adder	I	1					D		(I					
										1	1200.00	кер	eated F	enectio	ns aio	ng a lo	ussy iine	5	
	Unit		VS	WR			VS	WR											
	Impulse		Sou	irce	Ca	ble	LO	ad		1	1000.00								
	(Dirac) of δt		4.00E+00	:1			1.00	:1			800.00								
	of		0.25				1.00												
	amplitude										600.00								
	of 1	Γ=	0.60			Γ=	0.00				400.00								
											200.00								
	Signal =	1	Watt		Atten		Reflect	Load	Power										
	Time int		mWatts	dbm	Loss (db)	dbm	mWatts	mWatts	lost in cbl		0.00					_	_		
	0		1000.00	30.00	-	30.00	0.00	1000.00				0 1 2	3	4	5 6	7	8	9 10	
	1		0.00	-33.01 -35.23	-	-33.01 -35.23			0.00					Source	e 🔳 Load				
				-98.24		-98.24	0.00	0.00	0.00										
	2		0.00	-100.46	1	-100.46	0.00	0.00					Powo	r to the	load (r	mWat	tc)		
	2		0.00	-163.47	1	-163.47	0.00	0.00	0.00				Powe	r to the	ioau (i	IIVVal	(S)		
	3		0.00	-165.69	]	-165.69	0.00	0.00			1200.00								
	4		0.00	-228.70		-228.70	0.00	0.00	0.00										
2	-		0.00	-230.92		-230.92	0.00	0.00			1000.00								
<u>.o</u>	5		0.00	-293.93		-293.93			0.00		1000.00								
Reflection				-296.14	0.00	-296.14	0.00	0.00											
ē	6		0.00	-359.15		-359.15			0.00		800.00								
Ē				-361.37	-	-361.37	0.00	0.00											
ž	7		0.00	-424.38	-	-424.38			0.00		600.00								
_				-426.60 -489.61	-	-426.60 -489.61	0.00	0.00	0.00		600.00								
	8		0.00	-485.01	-	-485.01			0.00										
				-554.84		-554.84	0.00	0.00	0.00		400.00								
	9		0.00	-557.06		-557.06			0.00										
			0.00	-620.07		-620.07	0.00	0.00	0.00		200.00								
	10		0.00	-622.29		-622.29	0.00	0.00			200.00								
							0.00	0.00	0.00										
											0.00								
		0	dBW		Total	Power Tra	nsmitted =	1000.00	0.00			1 2 3 4	156	891	0 11 12	13 14 :	15 16 17	18 19 20 2	1 2
	smitter Zo	30	dBm																
Z =	50						Total p	ower =	1000.00	mWatts									
					Milli-Watt	s													
VSWR =	0.019607843		0.00		0.00		0.00												
					0.00			1000.00	1000.00	mMatta									
					0.00			1000.00	1000.00	mvvatts									

# Confirming the cable constants of a Sucoflex 104E coax cable



#### SUCOFLEX\_104

Cable design



	Description	Diameter
1. Centre conductor	Solid silver-plated copper wire	
2. Dielectric	Low density PTFE	
3. 1st outer conductor	Silver-plated copper tape, wrapped	
<ol><li>2nd outer conductor</li></ol>	Silver-plated copper braid	
5. Jacket	Fluoroethylenepropylene, blue	5.50 mm

#### Electrical cable data

Impedance					50 Ohm
Operating frequency					26.5 GHz
Capacitance					87 pF/m
Velocity of propagation					77 %
Time delay					4.3 ns/m
Nom. attenuation*	coefficient a	0.2291	coefficient b	0.0071	
Max. attenuation*	coefficient a	0.2520	coefficient b	0.0078	
Max. operating voltage					2.6 kVrms
Min. screening effectiveness up to 18 GHz					90 dB

\*Attenuation calculation  $a_{25} = a \cdot \sqrt{f}(GHz) + b \cdot f(GHz)$ 

(dB/m)

# **Practical implications of SWR**

- The most common case for measuring and examining SWR is when installing and tuning transmitting <u>antennas</u>. When a transmitter is connected to an antenna by a <u>feed line</u>, the <u>driving point impedance</u> of the antenna must be resistive and matching the characteristic impedance of the feed line in order for the transmitter to see the impedance it was designed for (the impedance of the feed line, usually 50 or 75 ohms).
- The impedance of a particular antenna design can vary due to a number of factors that cannot always be clearly identified. This includes the transmitter frequency (as compared to the antenna's design or <u>resonant</u> frequency), the antenna's height above the ground and proximity to large metal structures, and variations in the exact size of the conductors used to construct the antenna.
- When an antenna and feed line do not have matching impedances, the transmitter sees an unexpected impedance, where it might not be able to produce its full power, and can even damage the transmitter in some cases.<sup>[5]</sup> The reflected power in the transmission line increases the average current and therefore losses in the transmission line compared to power actually delivered to the load.<sup>[6]</sup> It is the interaction of these reflected waves with forward waves which causes standing wave patterns,<sup>[5]</sup> with the negative repercussions we have noted.<sup>[2]</sup>
- Matching the impedance of the antenna to the impedance of the feed line can sometimes be accomplished through adjusting the antenna itself, but otherwise is possible using an <u>antenna tuner</u>, an impedance matching device. Installing the tuner between the feed line and the antenna allows for the feed line to see a load close to its characteristic impedance, while sending most of the transmitter's power (a small amount may be dissipated within the tuner) to be radiated by the antenna despite its otherwise unacceptable feed point impedance. Installing a tuner in between the transmitter and the feed line can also transform the impedance seen at the transmitter end of the feed line to one preferred by the transmitter. However, in the latter case, the feed line still has a high SWR present, with the resulting increased feed line losses unmitigated.
- The magnitude of those losses are dependent on the type of transmission line, and its length. They always increase with frequency. For example, a certain antenna used well away from its resonant frequency may have an SWR of 6:1. For a frequency of 3.5 MHz, with that antenna fed through 75 meters of RG-8A coax, the loss due to standing waves would be 2.2 dB. However the same 6:1 mismatch through 75 meters of RG-8A coax would incur 10.8 dB of loss at 146 MHz.<sup>[5]</sup> Thus, a better match of the antenna to the feed line, that is, a lower SWR, becomes increasingly important with increasing frequency, even if the transmitter is able to accommodate the impedance seen (or an antenna tuner is used between the transmitter and feed line).
- Certain types of transmissions can suffer other negative effects from reflected waves on a transmission line. Analogue TV can experience "ghosts" from delayed signals bouncing back and forth on a long line. FM stereo can also be affected and digital signals can experience delayed pulses leading to bit errors. Whenever the delay times for a signal going back down and then again up the line are comparable to the modulation time constants, effects occur. For this reason, these types of transmissions require a low SWR on the feed line, even if SWR induced loss might be acceptable and matching is done at the transmitter.

# Review

- *Standing waves* are waves of voltage and current which do not propagate (i.e. they are stationary), but are the result of interference between incident and reflected waves along a transmission line.
- A **node** is a point on a standing wave of *minimum* amplitude.
- An *antinode* is a point on a standing wave of *maximum* amplitude.
- Standing waves can only exist in a transmission line when the terminating impedance does not match the line's characteristic impedance. In a perfectly terminated line, there are no reflected waves, and therefore no standing waves at all.
- At certain frequencies, the nodes and antinodes of standing waves will correlate with the ends of a transmission line, resulting in *resonance*.
- The lowest-frequency resonant point on a transmission line is where the line is one quarter-wavelength long. Resonant points exist at every harmonic (integer-multiple) frequency of the fundamental (quarter-wavelength).



Any questions No!!! then Time for Tea

The End